

# Conditioning of Hard Tools by Ultra Short Pulsed Lasers

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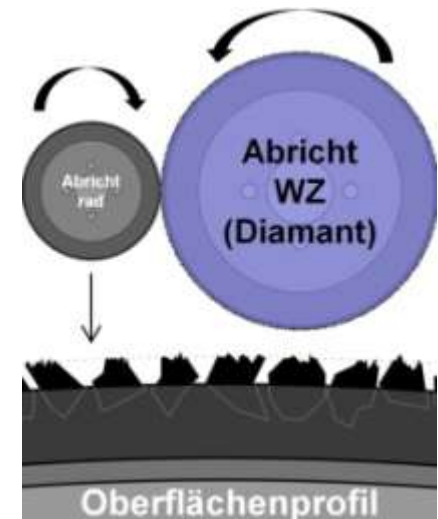


- Laser touching of dressing wheels
- Laser machining of PCD-tools
- Laser ablation of diamonds
- Laser conditioning of grinding wheels
- Laser structuring of cutting inserts
- Laser process simulation
- Conclusions

## Comparison of conventional- & laser-dressing process:

### ■ Conventional grinding machining:

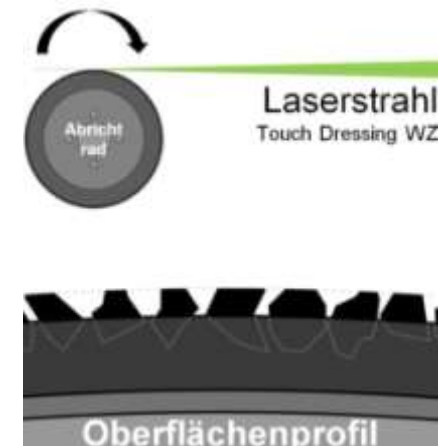
- Machining sequence: Dressing tool → dressing wheel → grinding wheel
- Diamond to diamond machining
- Material removal by micro cracks and grain break out



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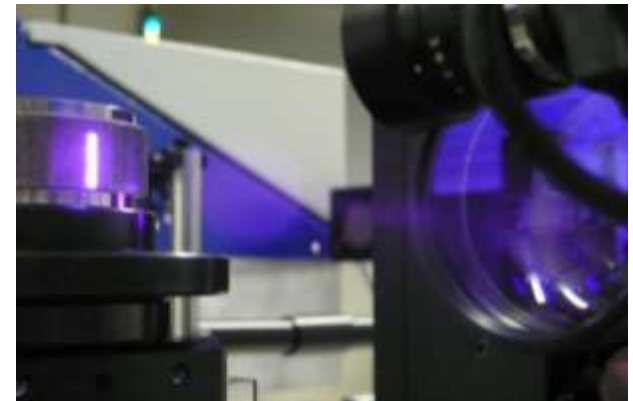
### ■ Laser machining:

- Machining sequence: Laser beam → dressing wheel → grinding wheel
- Laser beam tangential to the dressing wheel
- Diamond grains are precisely cut (no cracking!)
- Goals:
  - Adjusting a defined contact area → cutting of grain tips
  - Machining of a defined topography on the outer surface
  - Remove negative flank angles from the grain



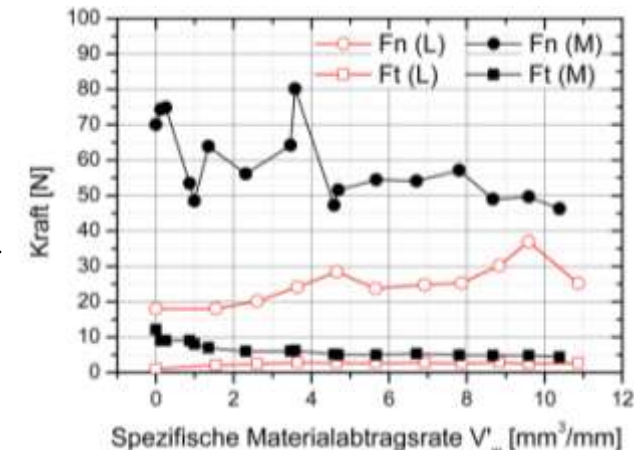
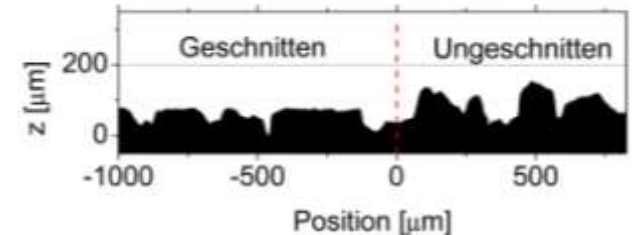
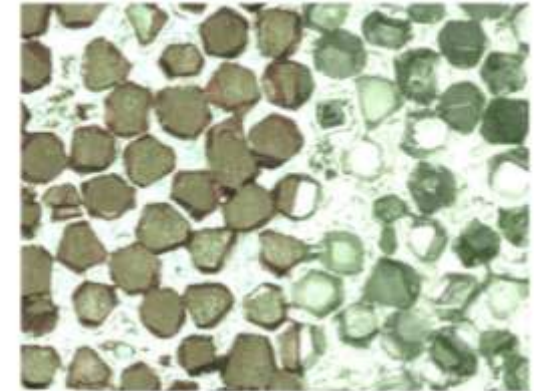
## Evaluation of touch dressed wheels:

- Cylinder roll / material:
  - Industry diamond Type IIa
  - Grain size D181
  - Nickel bonded
- Tangential laser machining:
  - Cutting of the grain protrusion
  - The bonding layer is not touched
  - Used wavelength:  $\lambda = 343, 1030 \text{ nm}$
- Dressing of a grinding wheel:
  - Grinding machine: Studer S31
  - Dressing a SiC-grinding wheel
  - Force measurements by a rotating Dynamometer

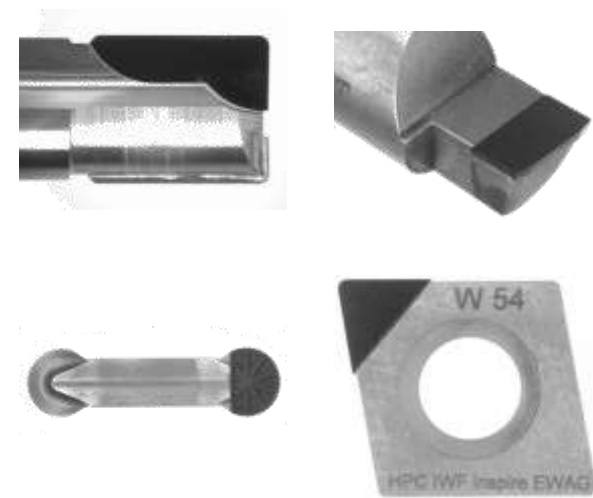


## Results of the evaluation:

- Selective machining of the area:
  - Problem-free machining by laser
  - All grains are machined with positive flank angle & without micro cracks
  - Process speed > 2 – 5 x higher than conventional dressing
  - No thermal nor mechanical damage of bonding layer
- Analysis of surface roughness:
  - Laser machined dressing tools shows slightly better results
- Process forces:
  - Tangential forces: **Laser** < Mechanical dressing
  - Normal forces: **Laser** << Mechanical dressing

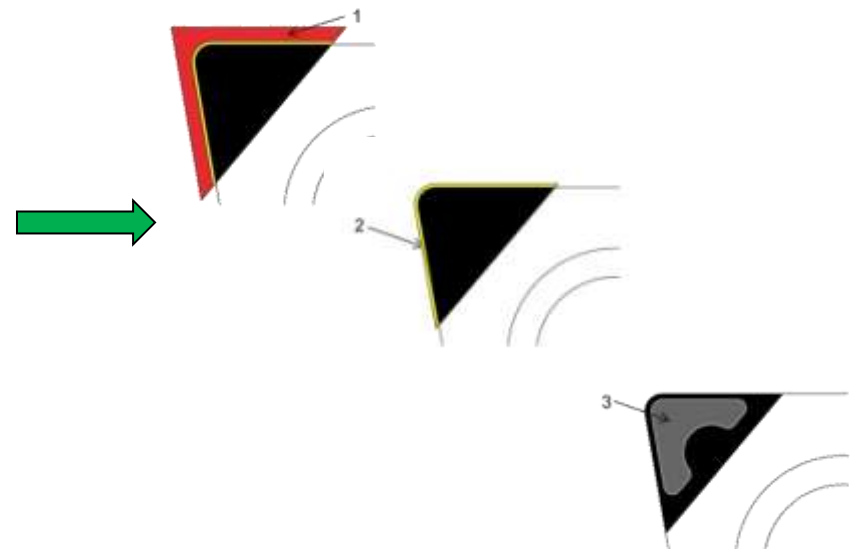


- High performance tools often shielded / coated by PCD, CVD, cBN
- Advantages of laser machining of PCD tools & inserts:
  - Individual adaptation to defined process → unlimited variety
  - Cutting geometry in 2D & 3D possible
  - Complex chip surface & chip breaking area in 3D-machining
  - Mostly single stage process compared to conventional process





- Sequence of laser machining an insert:

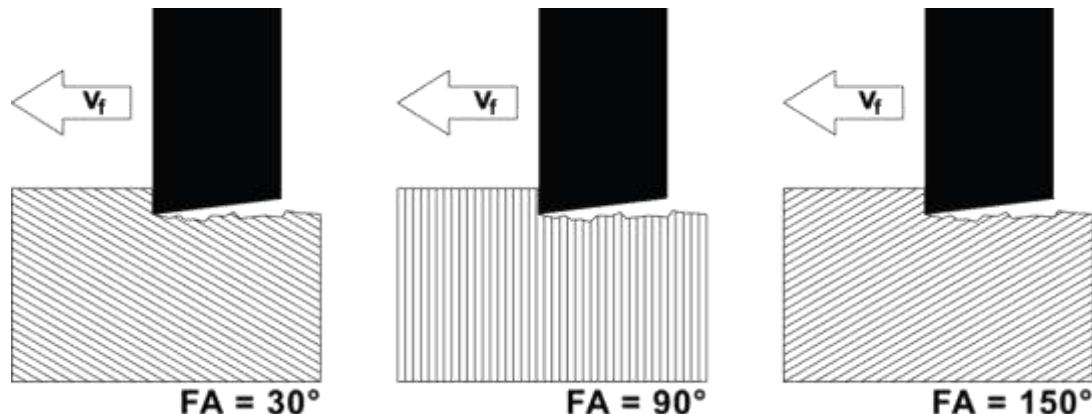
1. Removing of overlaying contour
2. Machining of the cutting edge geometry:
  - Flank face
  - Rounding of the cutting edge
3. Machining of optional geometry elements:
  - Rake face
  - Chip breaker
  - Chamfer radius





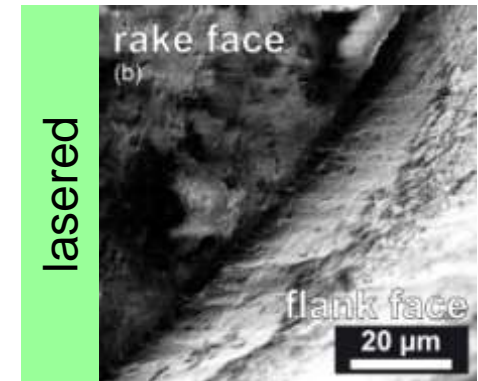
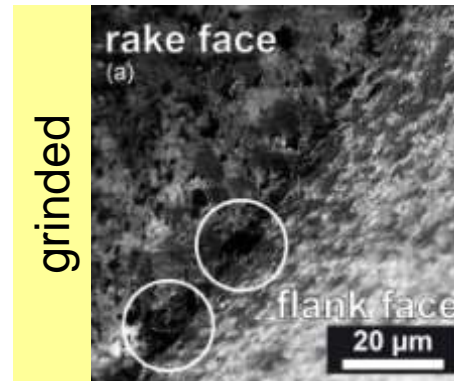
## Validation & comparison of laser- & conventional-machined PCD tools:

- Comparison of grinded & lasered inserts 
- Validation by means of turning CRP material with 3 different fiber orientations
- Evaluating of: 
  - cutting forces
  - cutting edges
  - machining time

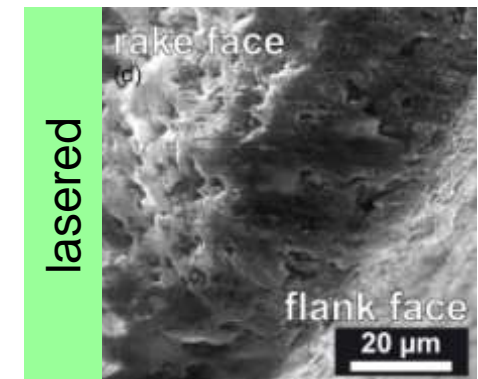
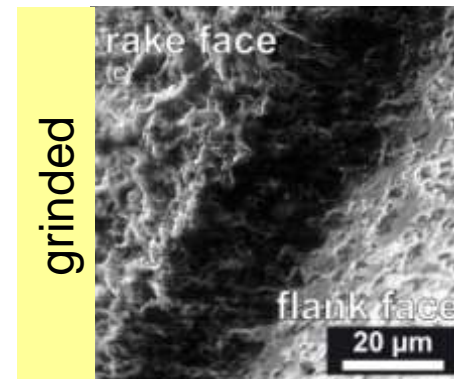


## Results of the validation:

- New grinded cutting edges:
  - Grain breakout → size of  $\frac{1}{2}$  grain
- New lasered cutting edges:
  - No grain breakout
  - Good chipping of the cutting edge



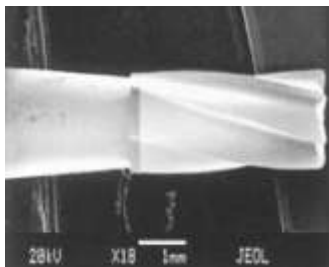
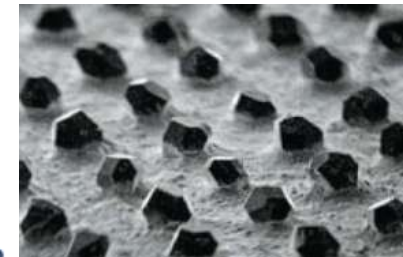
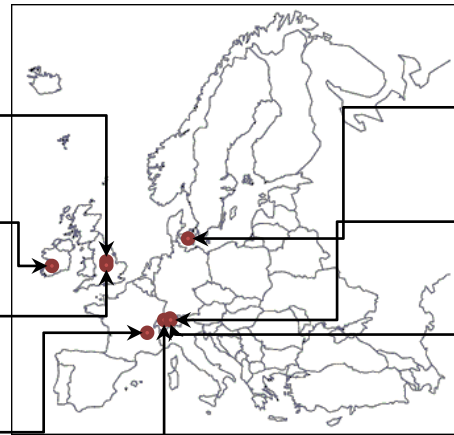
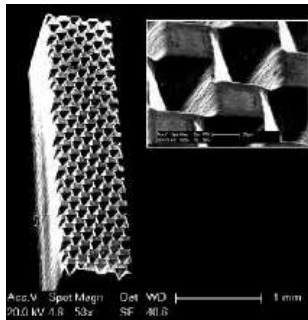
- 
- Worn cutting edges:
    - Similar for grinded & lasered inserts:
      - Flank-wear land width
      - Wear behavior
      - At a cutting depth of 1 grain size → identical wear



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- Identical machining time for grinding and lasering an insert



## Enabling advanced functionalities of **D**iamond and other ultra-hard materials by **I**ntegrated **P**ulsed **L**aser **A**blation **T**echnologies



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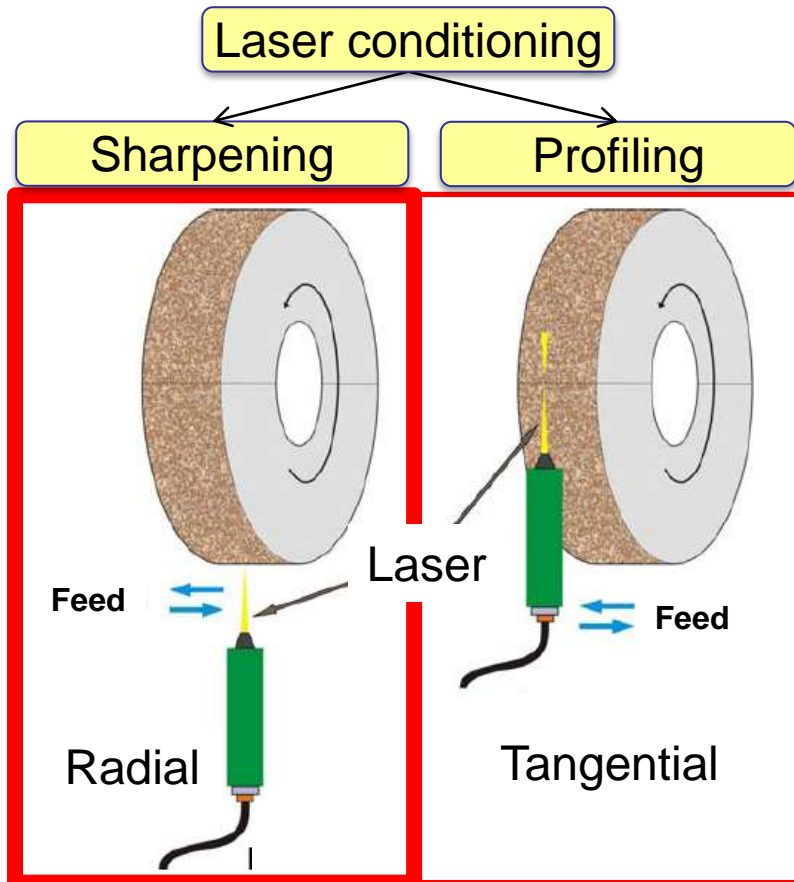


**FP7-2012-NMP-ICT-FoF**  
FoF.NMP.2012-7 - New technologies for casting,  
material removing and forming processes



- **Goal: Generate a cBN grinding wheel topography by laser machining**

## Principle:

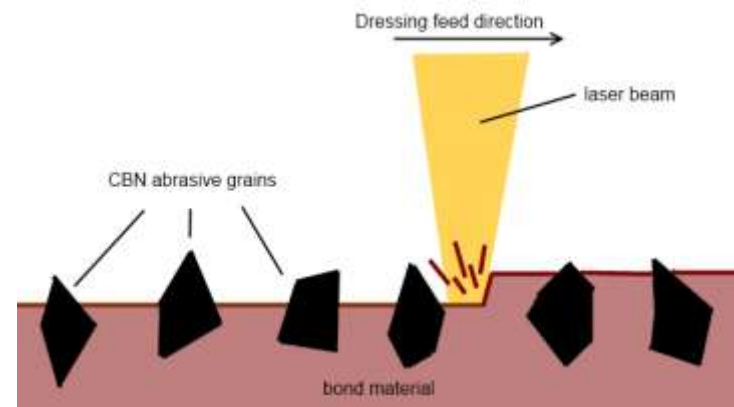


- **Laser source:**

- Short pulsed fiber laser: Rofin Lasag QFS 50
- $P = 50 \text{ W}$ ,  $t_P = 150 - 200 \text{ ns}$
- $e_P = 1 \text{ mJ @ } 50 \text{ Hz}$

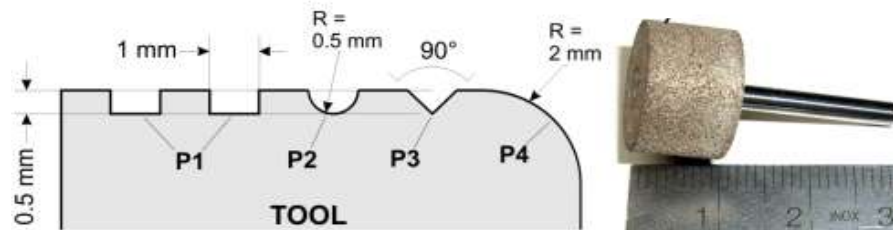
- **Cutting head:**

- Fixed focal length with process gas
- $f = 150 \text{ mm}$ ,  $d_{\text{foc}} = 50 \mu\text{m}$
- Process gas: Pressured air (5 bar)

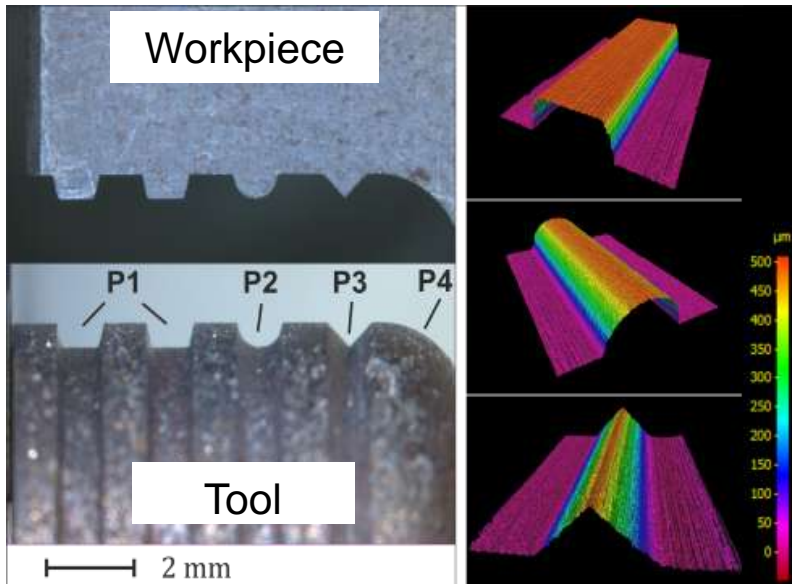


## ■ Example: Laser conditioning of a cBN grinding pin

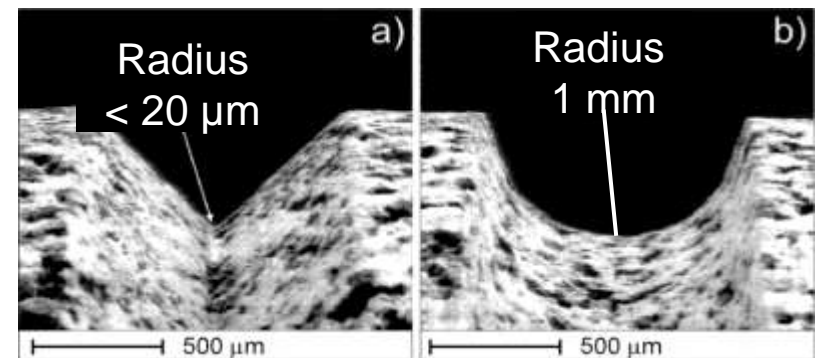
### Tool geometry:



### Tool & Workpiece after machining:

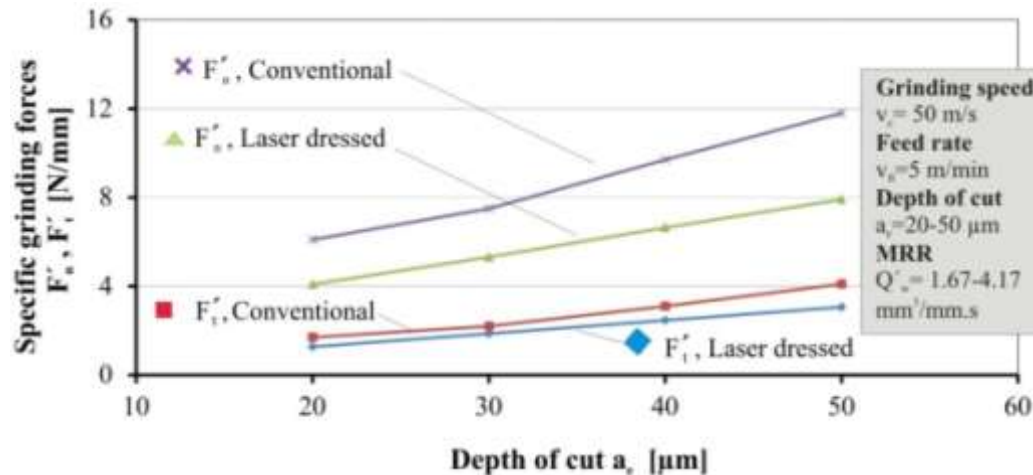


### Details of the lasered tool:



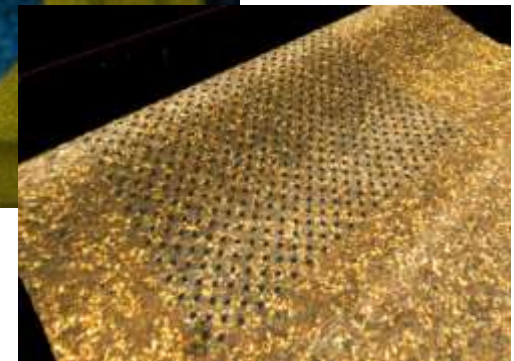
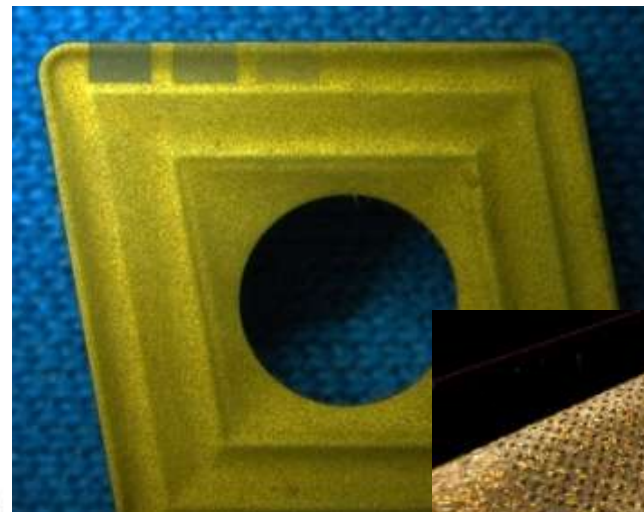
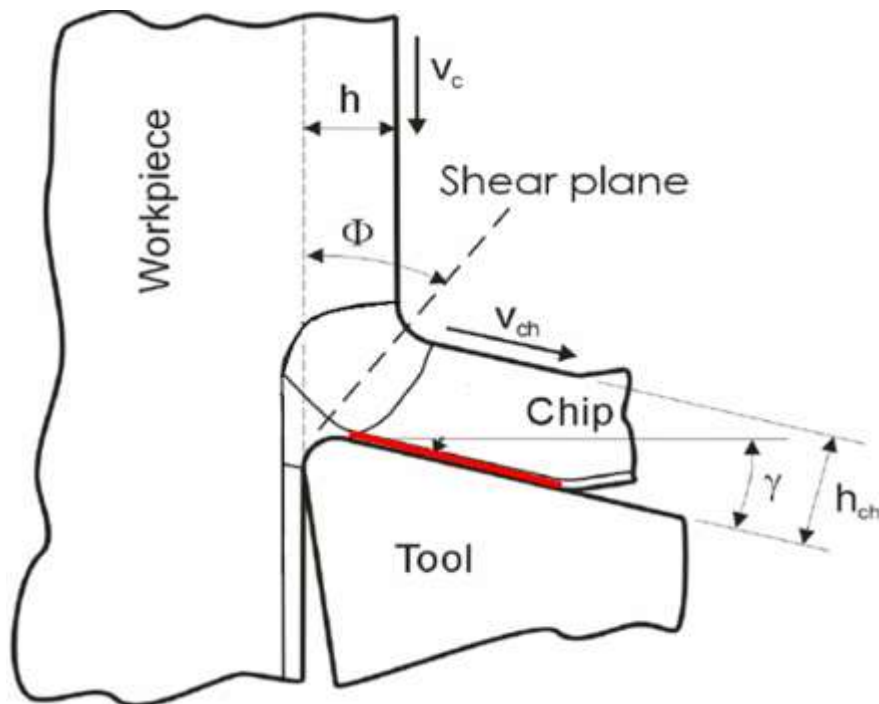
## Results of laser conditioning process:

- Tangential- and normal forces ( $F_t$ ,  $F_n$ )
  - Clearly lower compared to conventional process
  - Identical difference to conventional force curves even at high material removal rates
  - Slightly higher wear due to higher grain protrusion



- Stable grinding conditions after run in
- Compact surface due to tangential profiling
- No grain damage in consequence of laser machining

- Goal: Minimizing of chip friction on cutting inserts
  - Wear reduction
  - Better chip flow
  - Better surface quality
- Task: Structuring of the chip surface to built lubricant pockets



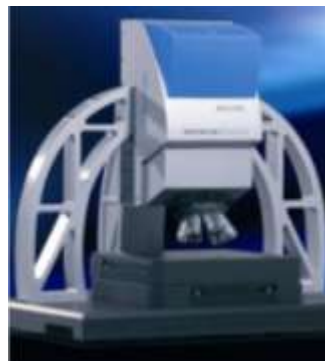


## Laser machine TRUMPF VC5

- Hardware specification
  - $\lambda$  : 355 nm
  - Laser type: Nd: YVO4
  - f : 160 mm
  - Focus dia.: ~25  $\mu\text{m}$
- Software
  - Marking software
  - CAD editor
  - Laser parameter administration

## Optical measurement

- Alicona Infinite focus



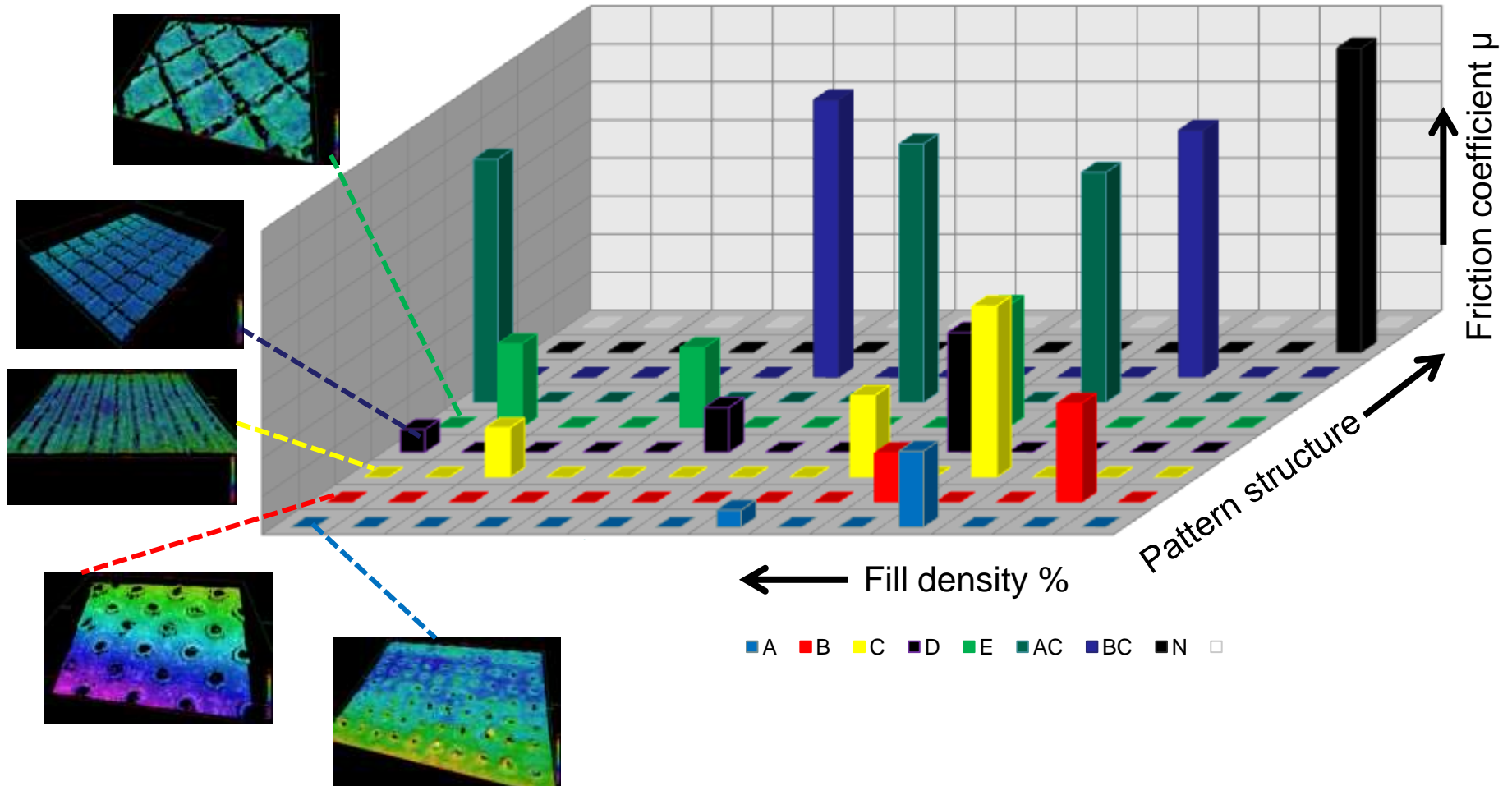
## Tasks for structuring optimisation

- Focal plane and beam diameter:
  - Ellipticity
  - Energy density
- Optimization of laser parameters:
  - Power
  - Velocity
  - Frequency
  - Pulse width and number of pulses
  - Internal laser parameter
  - Precision
  - Hatching
- Multiple marking and controlling depth
- Change of optics

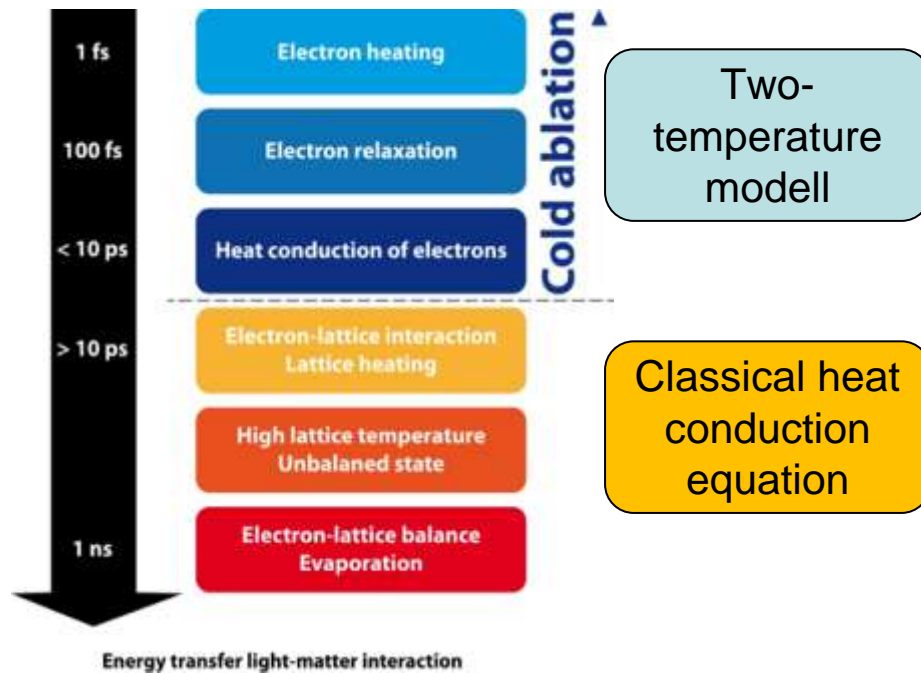


## Results of cutting experiments:

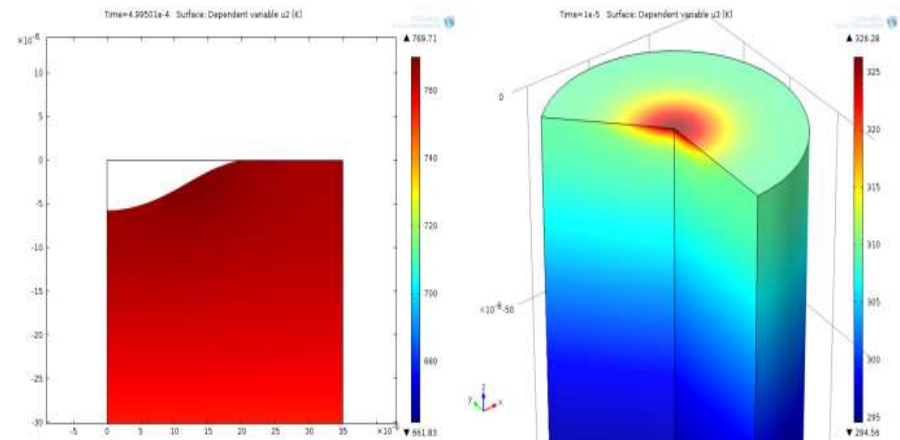
- Relation between fill density, pattern structure & friction coefficient



Pulse time dependent ablation characteristic:



Simulation result of a 10 ps-laser process:



- Conclusions for laser ultra short pulse machining of ultra hard surfaces:
  - The process is convenient for grain and insert geometries
  - Smallest cutting edge radii accessible:
    - Single grain type IIa  $r_K > 4 \mu\text{m}$
    - PCD, CVD-D  $r_K > 2 \mu\text{m}$
  - Surface roughness  $R_a < 0.2 \mu\text{m}$
  - No thermal damage of the machined material → best cutting edge quality
  
- Trends for laser process development:
  - From tool inserts to highly complex 3D geometries
  - Laser beam guidance:
    - Higher scanning velocities
    - Accuracy of tool center point (TCP)
    - Synchronisation (time) with CNC axes

Thanks to ...

Many thanks to ...



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Confederazione Svizzera  
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Swiss Confederation

Federal Department of Economic Affairs,  
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