

Willkommen
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Bienvenue

Recent Developments of Joining Technologies for Ever-more Complex Industrial Requirements

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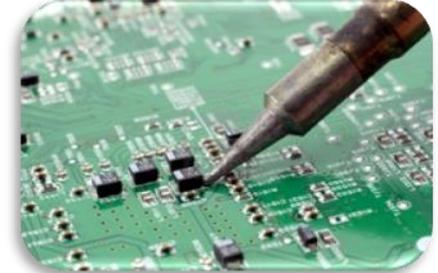
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Industrial requirements

- ✓ Joining of heat-sensitive materials and miniaturized components.
- ✓ Extended service lifetime of joint assemblies in harsh environments.

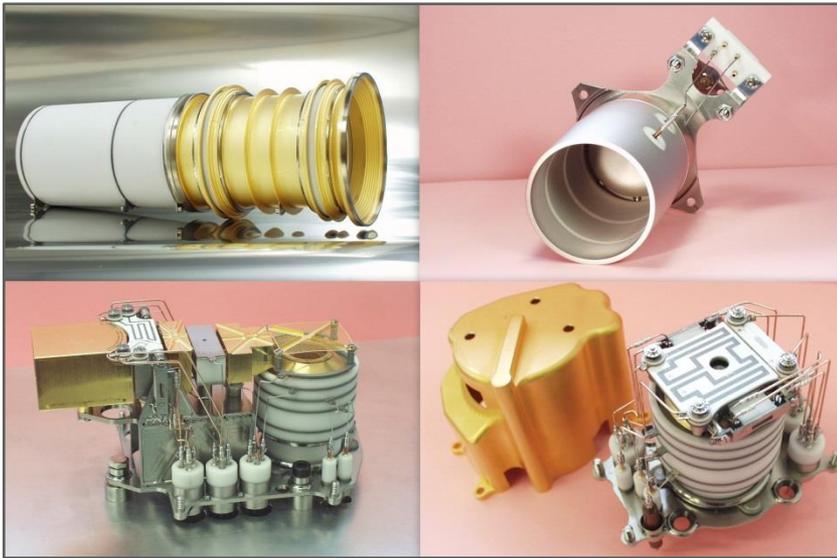
Process and service requirements

- ✓ Fast joining at ever-lower temperatures
- ✓ Long-term mechanical and chemical stability during operation
 - at elevated temperatures
 - under fast cyclic thermo-mechanical loading conditions.
 - in high shock and vibration environments.
 - in moisture, ionic liquids and reactive gas atmospheres (under high pressures).



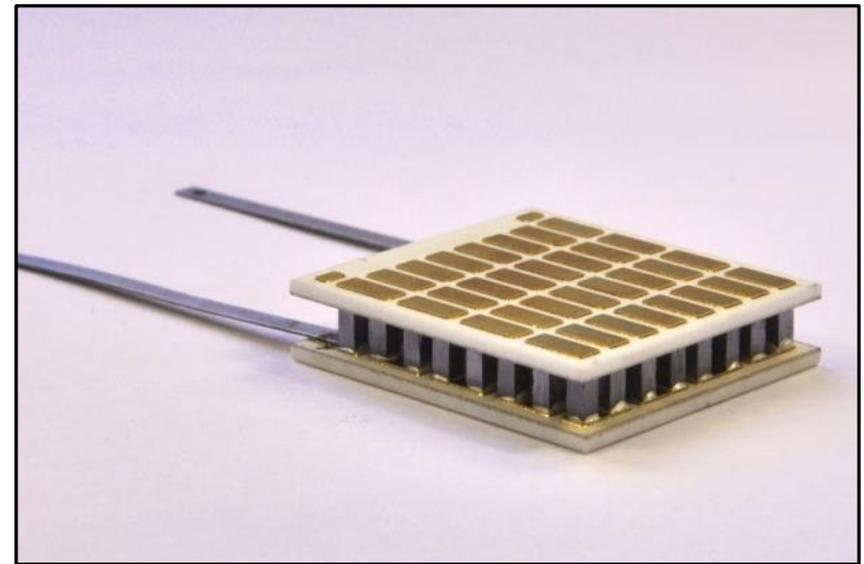
Harsh environments for joint assemblies

- ✓ Rapid thermal cyclic in the range of $-40\text{ }^{\circ}\text{C}$ up to $250\text{ }^{\circ}\text{C}$.
- ✓ Operation beyond $125\text{ }^{\circ}\text{C}$ in high shock and vibration environments.
- ✓ Operation in moistures and ionic liquids (i.e. high corrosion resistance).
- ✓ Operation in reactive gas atmospheres under high pressures.



Fabricated @ Empa:

*Ion-Optical Components for ROSINA RTOF
(University of Bern / ESA mission Rosetta)*



TLP-Bonded @ Empa:

Thermoelectric module for exhaust applications

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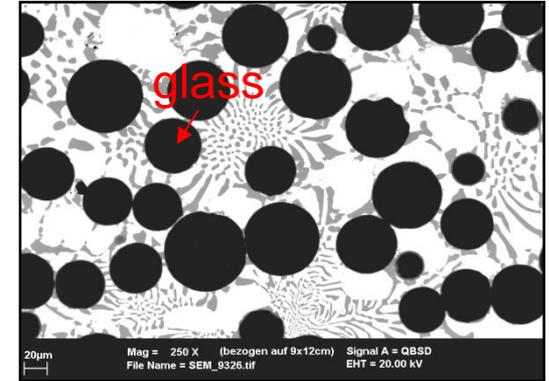
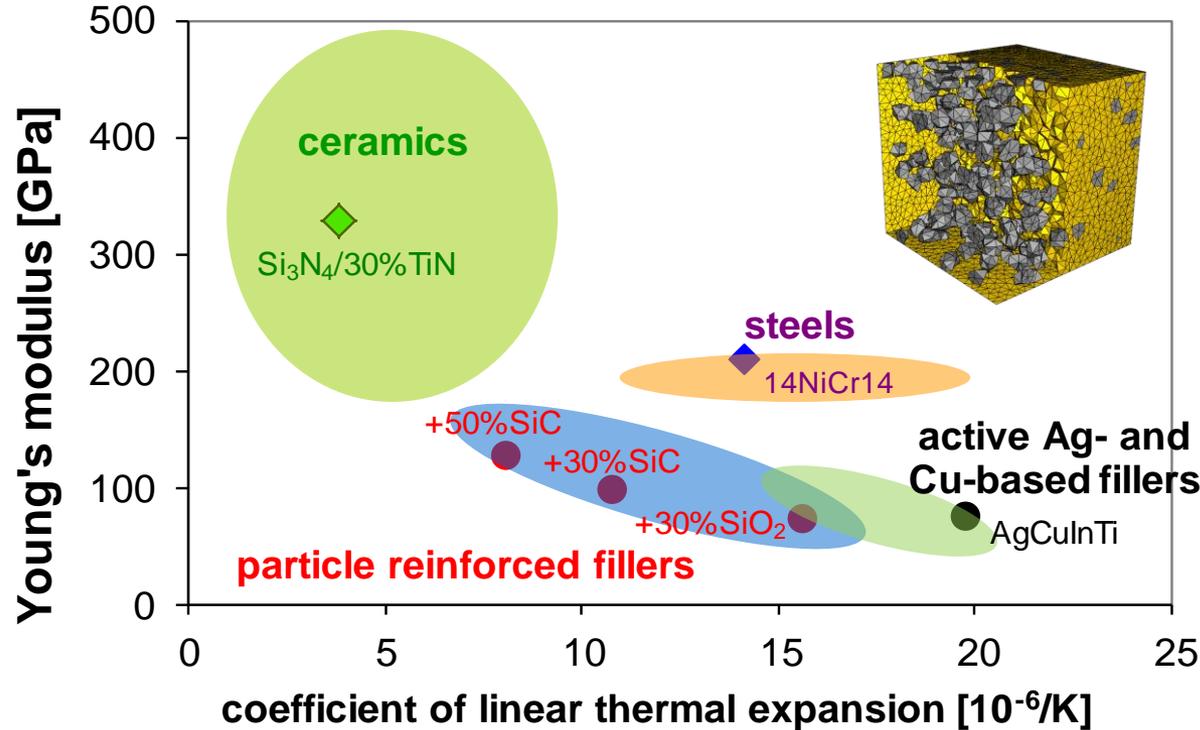
Laboratory for Joining Technologies & Corrosion

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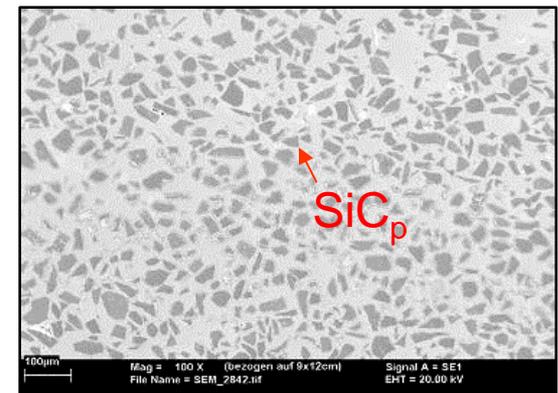


Materials Science & Technology

Application of particle-reinforced brazing fillers for improved mechanical performance



AgCuInTi/glass ($d=60\mu m$)



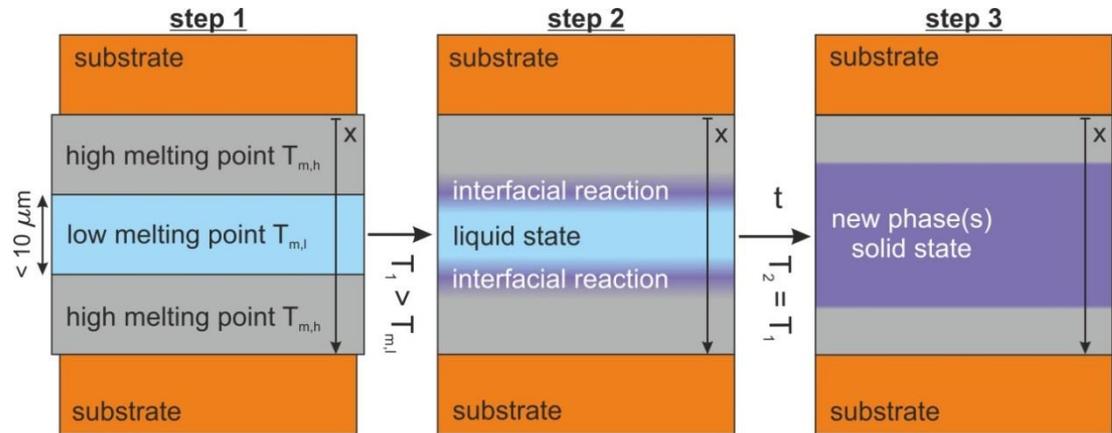
CuSnTiZr/SiC_p ($d=25\mu m$)

Particle reinforced brazing fillers provide tuneable physical properties, which can be tailored to reduce thermomechanical stresses of joint assemblies during operation.

Transient Liquid Phase (TLP) Bonding

Advantages of the TLP process

- Fast joining < 250 °C
- Operation >> 250 °C



Basic Principles of the TLP process

Common TLP systems

Low-melting-point metal

➤ Sn ($T_{m,l} = 232 \text{ }^\circ\text{C}$)

➤ In ($T_{m,l} = 157 \text{ }^\circ\text{C}$)



High-melting-point metal

Ag, Cu, Ni or Au

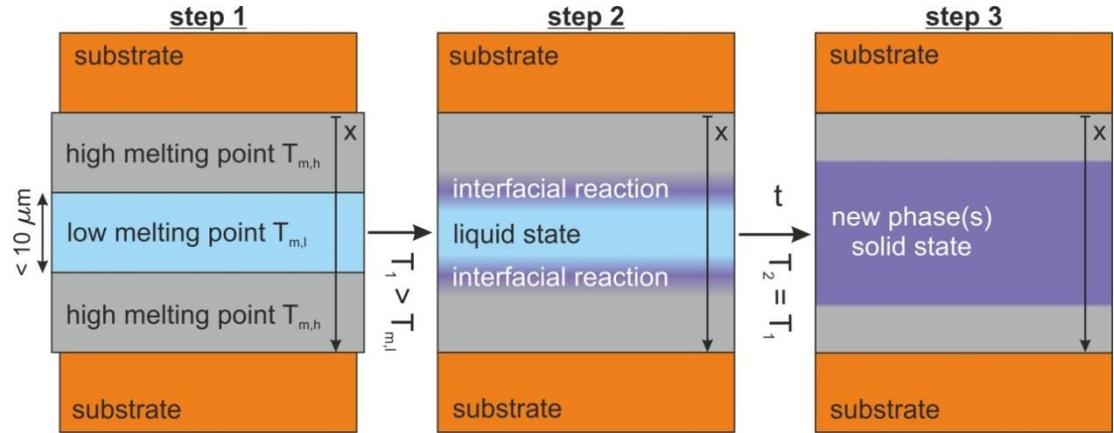
Process optimization issues

- Relative narrow (T, t)-processing windows
- Shrinkage porosity due to incomplete consumption of liquid Sn phase
- Kirkendall porosity (e.g. for CuSn)

Transient Liquid Phase (TLP) Bonding

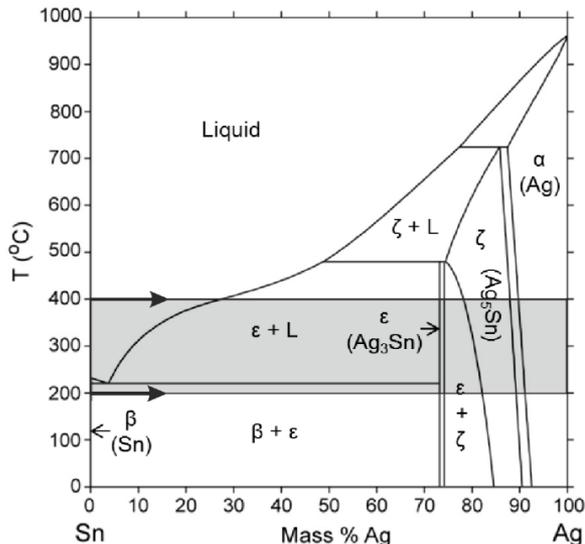
Advantages of the TLP process

- Fast joining < 250 °C
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Basic Principles of the TLP process

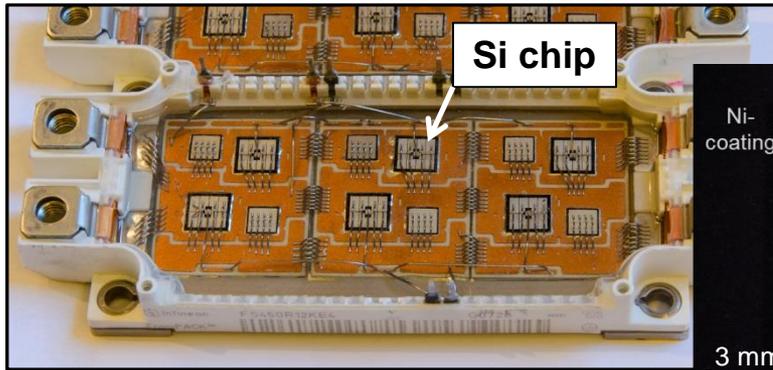
Example: Ag-Sn and Ni-Sn TLP bonding



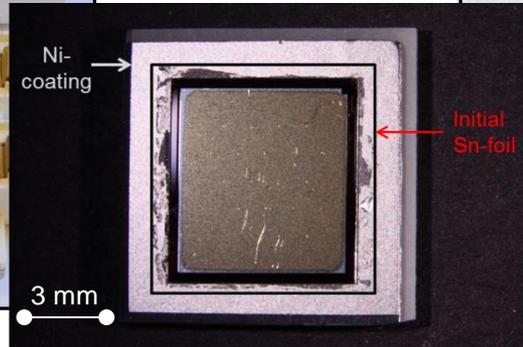
- ✓ Ag-Sn & Ni-Sn: $235\text{ °C} \leq T_{\text{process}} \leq 300\text{ °C}$
- ✓ Ag-Sn: formation of Ag_3Sn (ϵ) with $T_m = 480\text{ °C}$
- ✓ Ni-Sn: formation of Ni_3Sn_4 with $T_m = 794.5\text{ °C}$

Transient Liquid Phase (TLP) Bonding

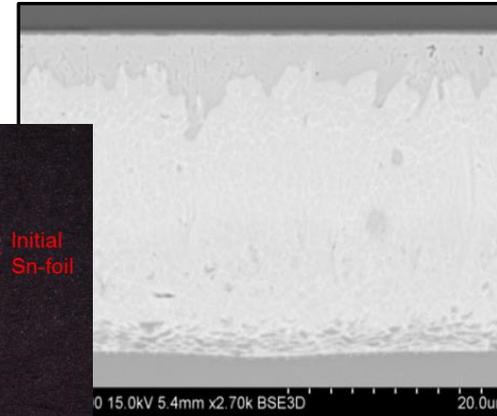
Ag-Sn TLP bonding for power electronics



Full IGBT module [source: Infineon]



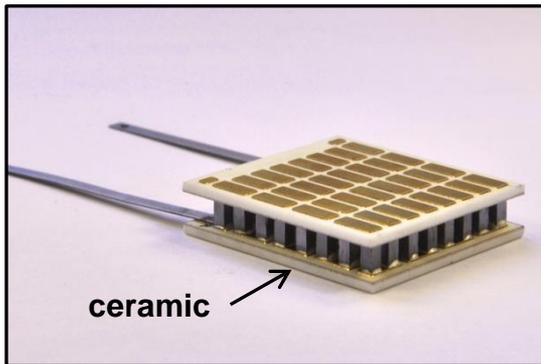
TLP-bonded Si chip [bonded @ Empa]



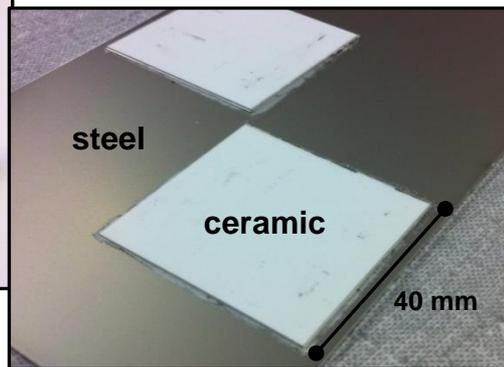
Cross-section of Ag-Sn TLP bond

- Si chip
- Ni_3Sn_4
- Ag_3Sn
- Ag

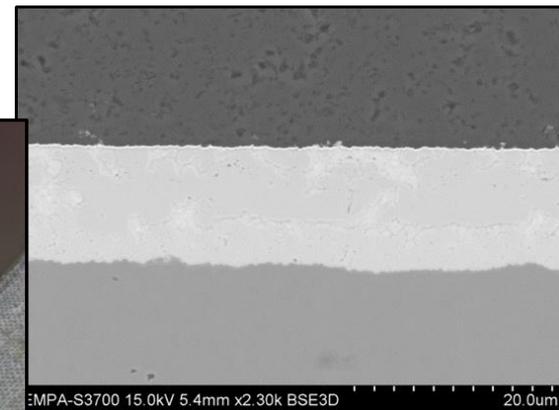
Ni-Sn TLP bonding for automotive applications



Thermoelectric module for exhaust applications



Large-area TLP bond [bonded @ Empa]

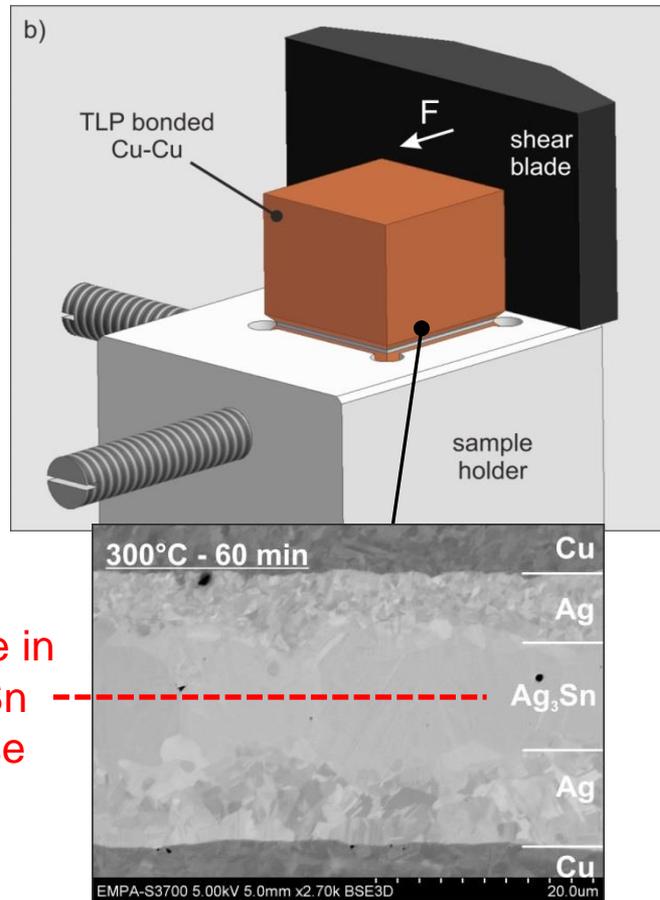


Cross-section of Ni-Sn TLP bond

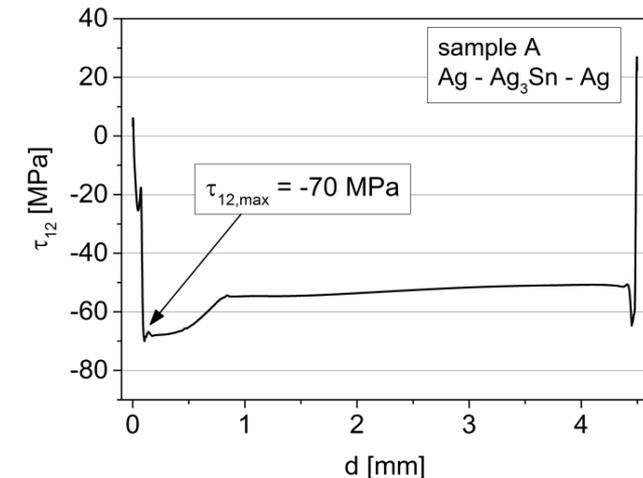
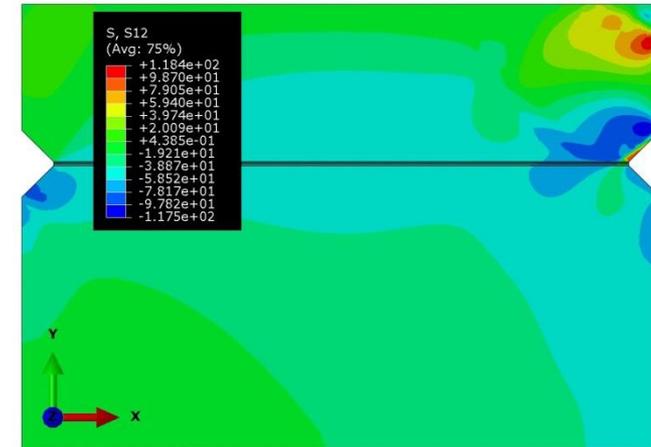
- Al_2O_3
- Ni_3Sn_4
- Ni

Shear strength of Ag-Sn TLP bonded Cu-Cu joints (no CTE mismatch)

Experimental



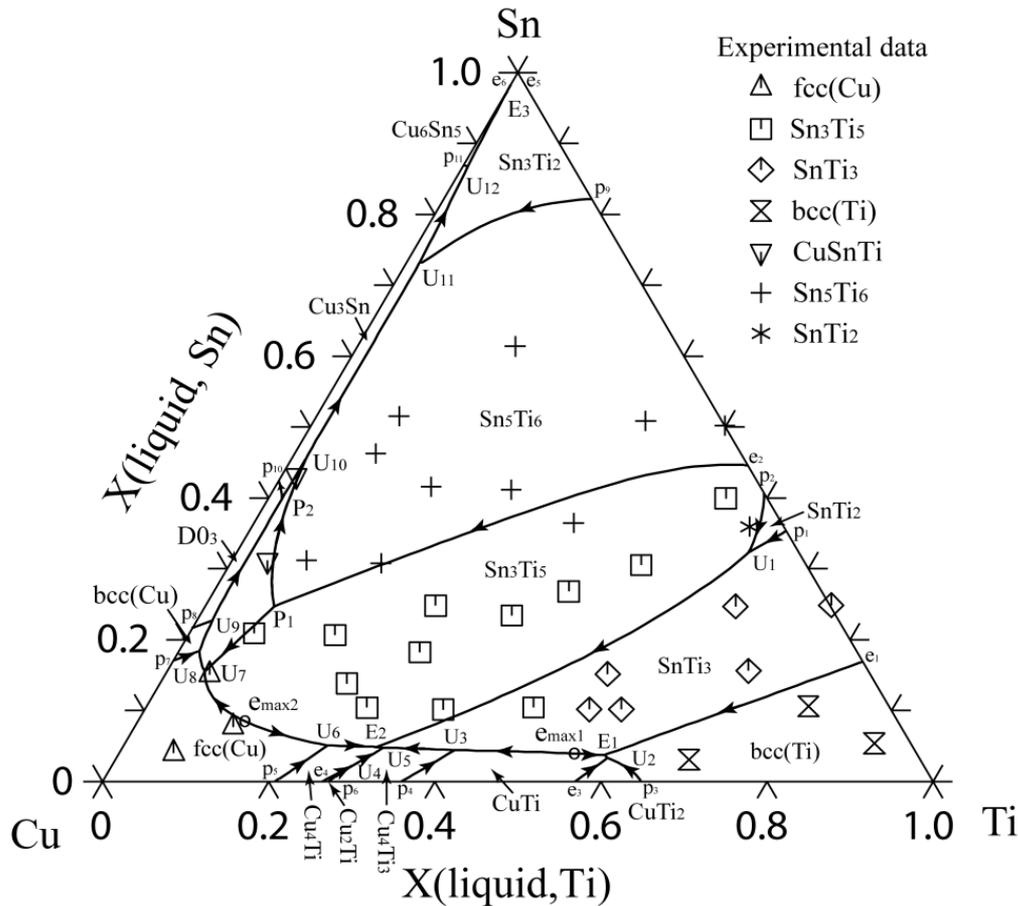
Finite-Element Modelling



$$\tau_{\text{mean}} = 60.7 \pm 7 \text{ MPa } (M = 0.5 \text{ Nm})$$

$$\tau_{\text{crit,loc}} = 70 \text{ MPa}$$

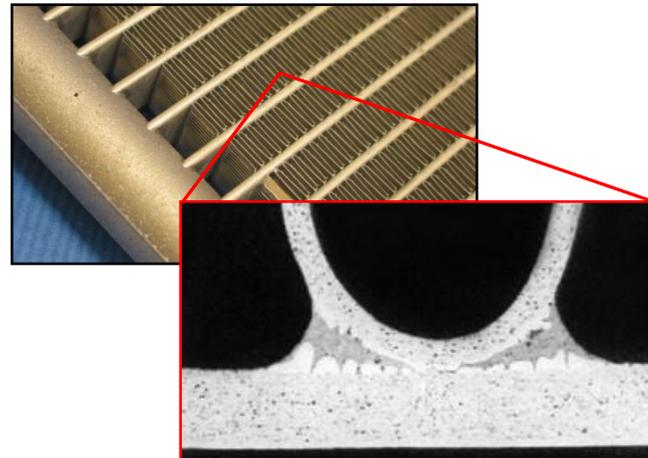
Conventional brazing and soldering technologies rely on **Bulk Alloy Design** to reduce eutectic melting points, promote wetting and optimize interface bond strengths.



Liquidus projection of the Cu-Sn-Ti diagram (by CALPHAD methods)



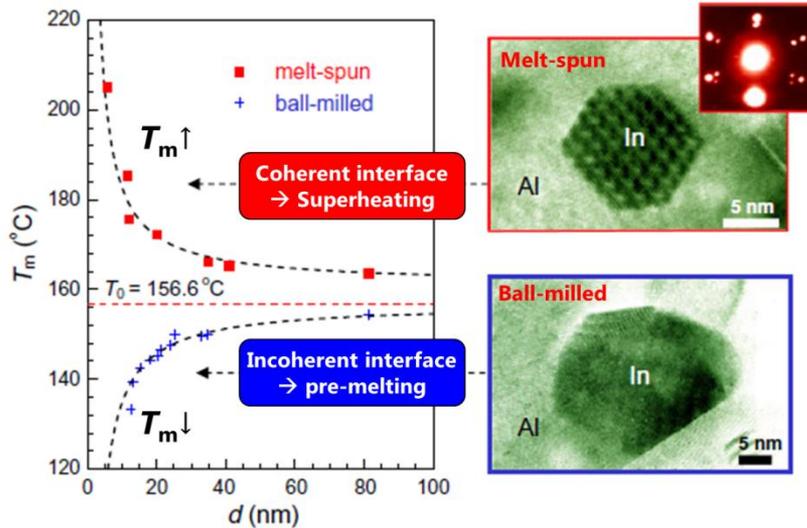
Joining of diamond or c-BN for high-performance cutting tools



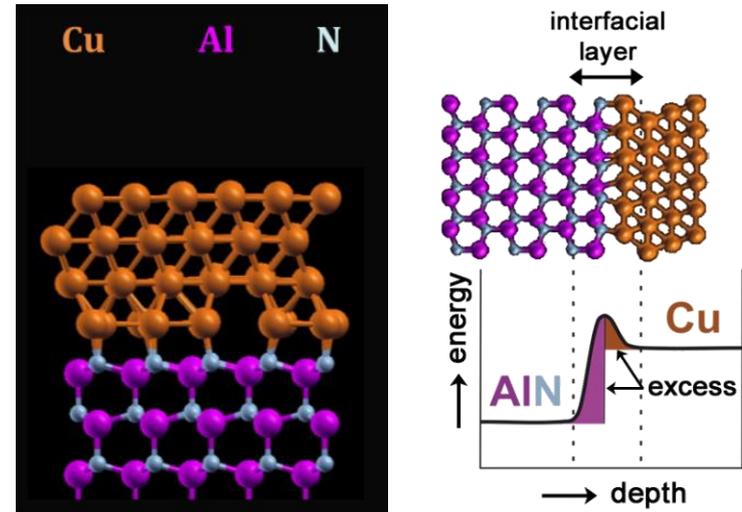
Joint assemblies in Al heat exchangers for automotive industries

Nano-joining technologies are based on **Nanostructured Filler Design**

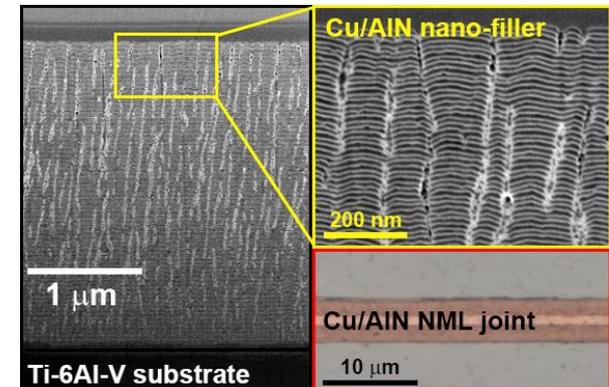
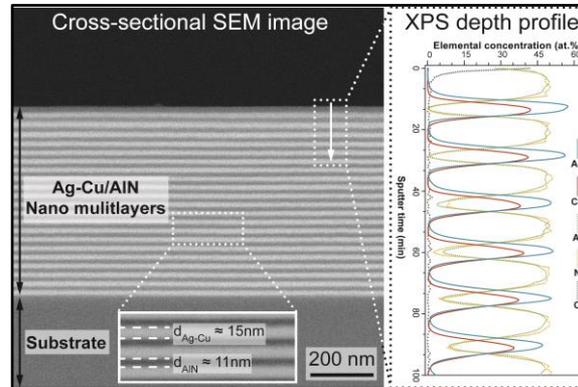
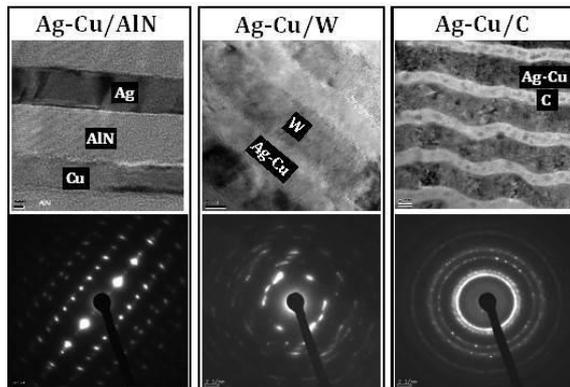
to tailor pre-melting, wetting and interfacial reaction kinetics by exploiting nano-scale effects



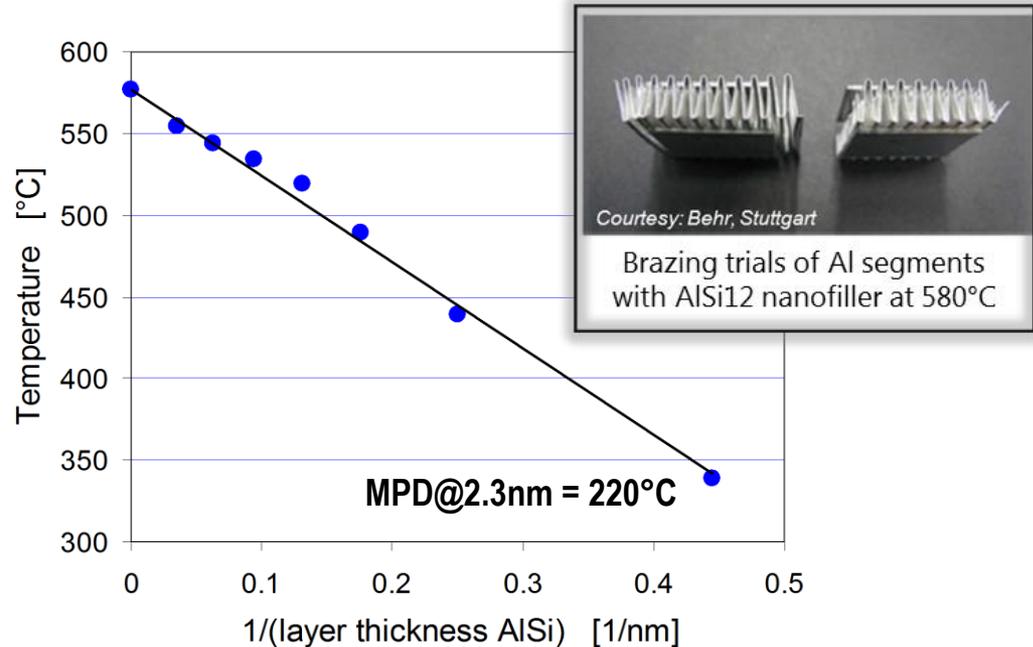
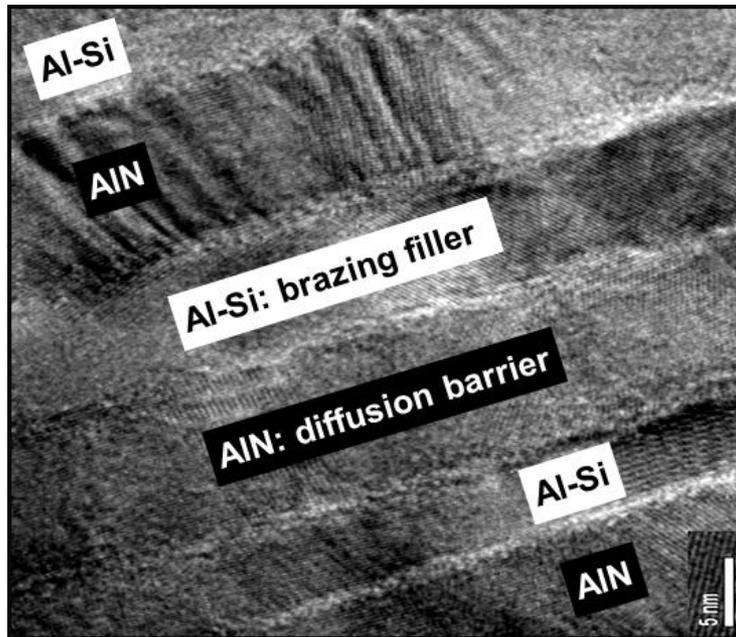
Interface engineering to promote interfacial pre-melting
[source: Lu & Jin, *Curr. Opin. Solid State Mater. Sci.* 5 (2001) 39]



Multi-scale modelling of defect structures and atomic mobilities at semi-coherent and incoherent interfaces [Empa]



Example: AlSi-AlN nano-fillers for low-temperature brazing of Al alloys
(Patent DE102008050433.5)

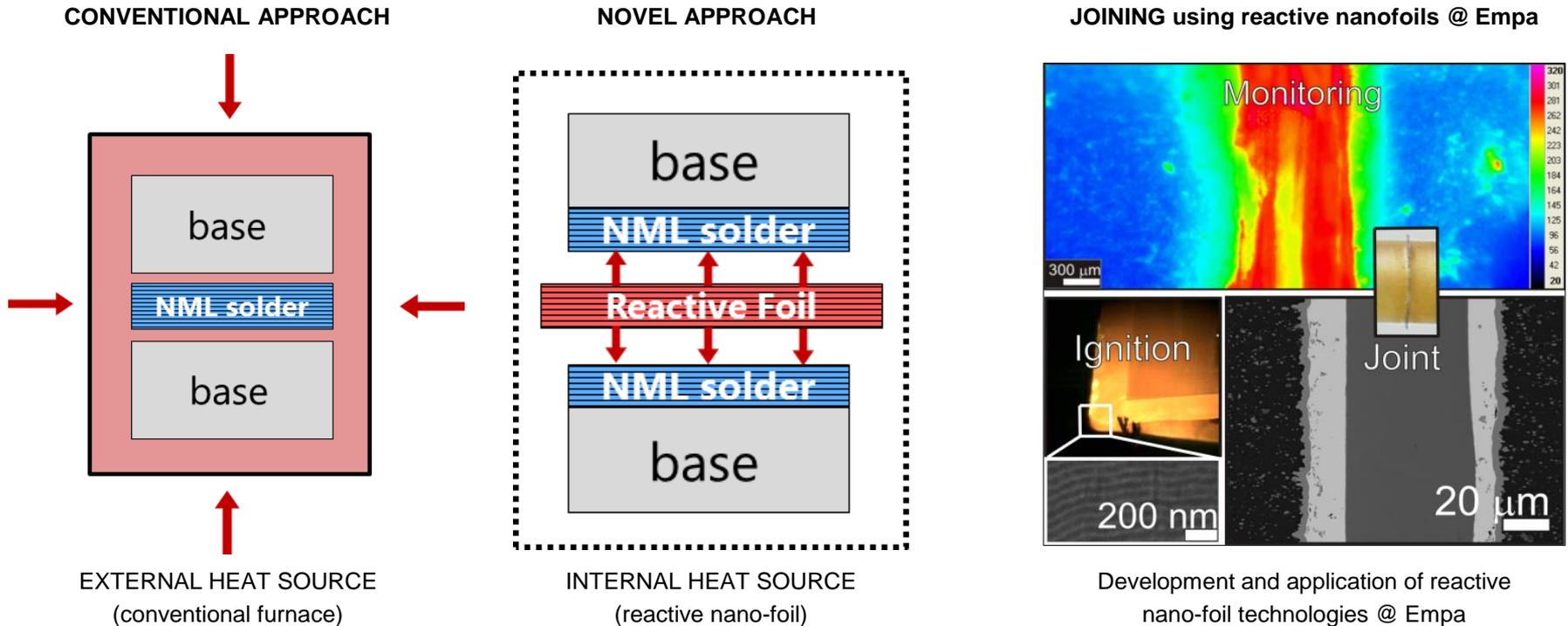


Ultra-thin Al-Si films sandwiched between inert AlN diffusion barriers exhibit size-dependent melting point depression (MPD)

Recent references on nano-joining research @ Empa

- *Copper-Based Nanostructured Coatings for Low-Temperature Brazing Applications*, Materials Transactions (2015).
- *Structural evolution of Ag-Cu nano-alloys confined between AlN nano-layers upon fast heating*, Physical Chemistry Chemical Physics (2015)
- *Interfacial design for joining technologies – An historical perspective*, Journal of Materials Engineering and Performance 23 (2014) 1608.

Combining nano-structured brazing fillers with reactive nano-foil technologies

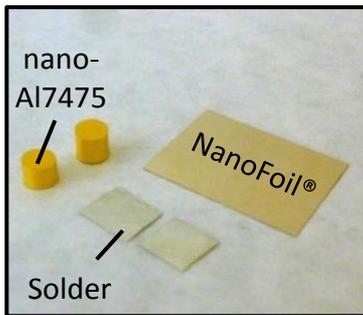
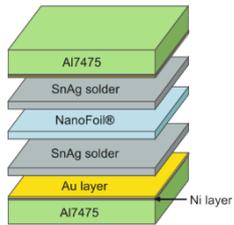


Advantages of reactive foil joining technologies

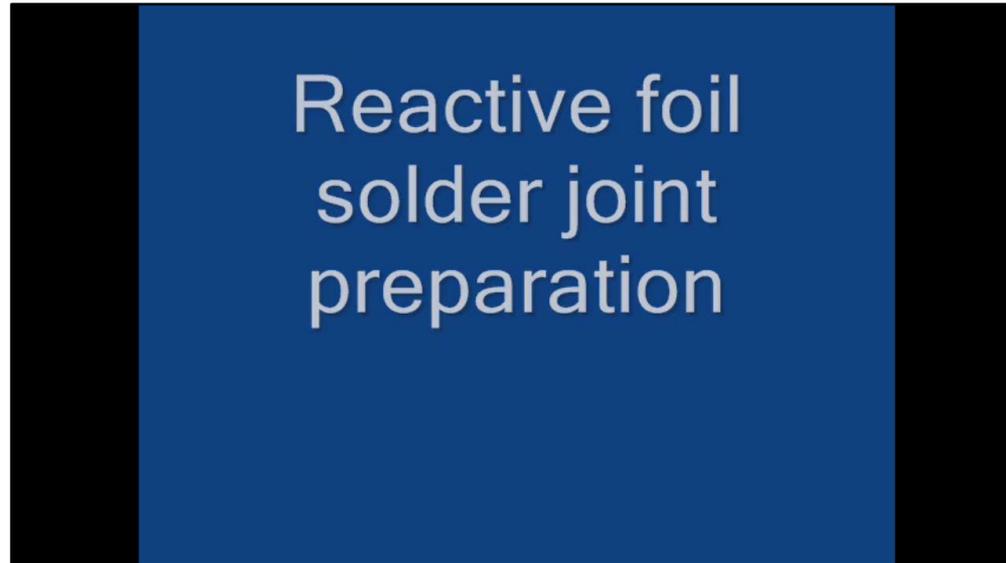
- No furnace needed!
- Fast joining at room-temperature in air or shielding gas.
- Heat is localized to bonded interface only, thus allowing joining of heat-sensitive materials

Example: Joining of nano-Aluminium using reactive Nano-Foil® technology

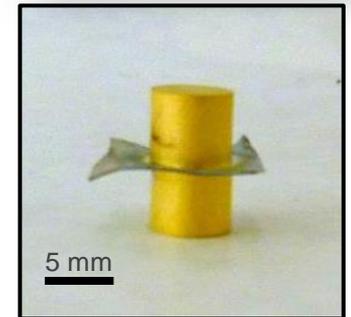
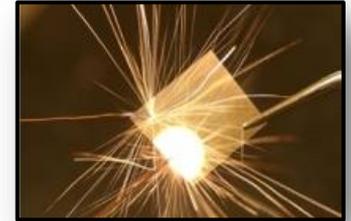
PREPARATION



JOINING PROCEDURE



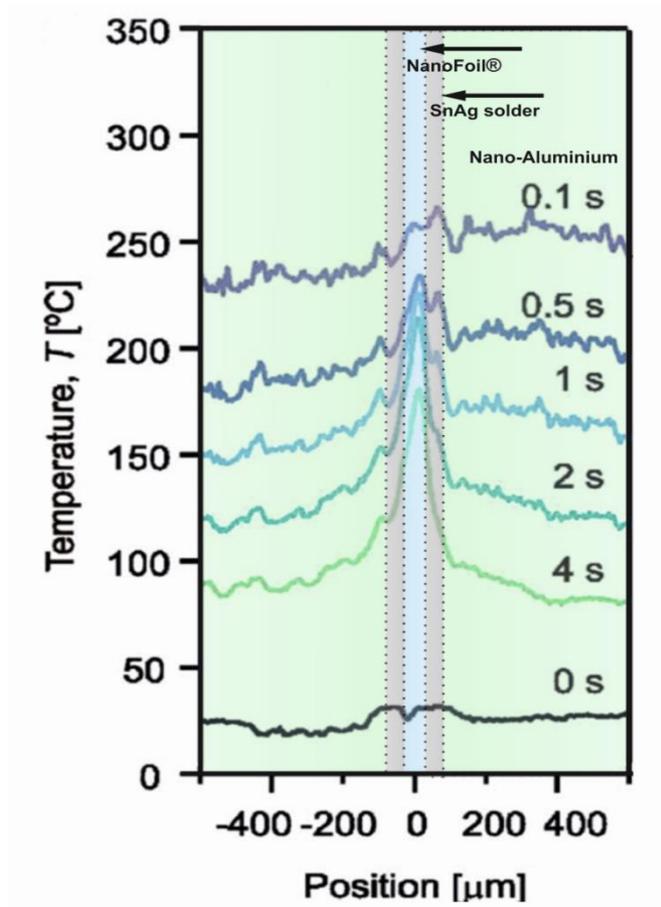
JOINT



Process characteristics

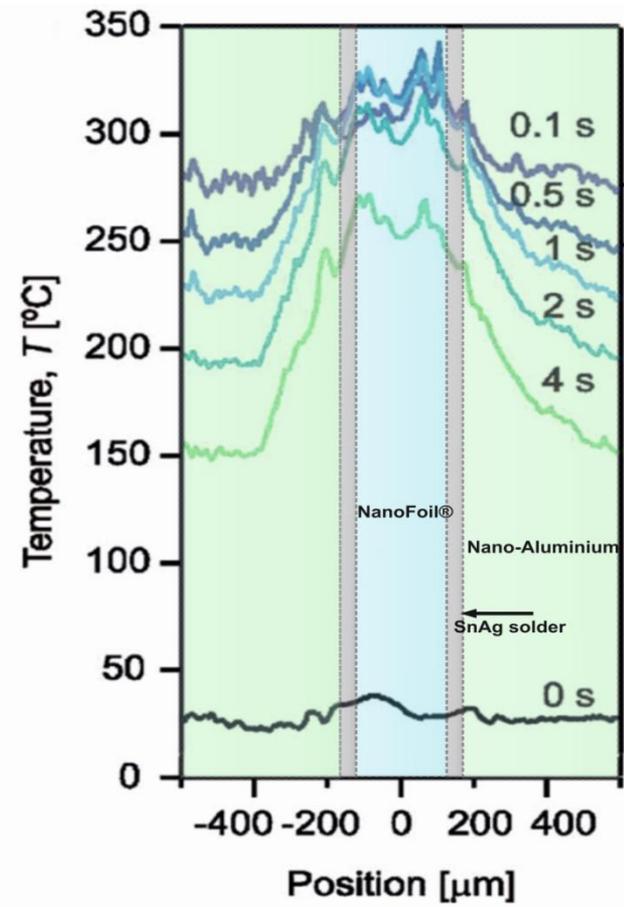
- Ni and Al nanolayers react to form Ni_3Al and/or NiAl (heat of reaction up to -52 kJ/mol).
- Local ignition at room temperature with electrical spark, laser pulse or hot filament.
- Self-propagating reaction front with a speed up to 30 m/s.

Example: Joining of nano-Aluminium using reactive Nano-Foil® technology



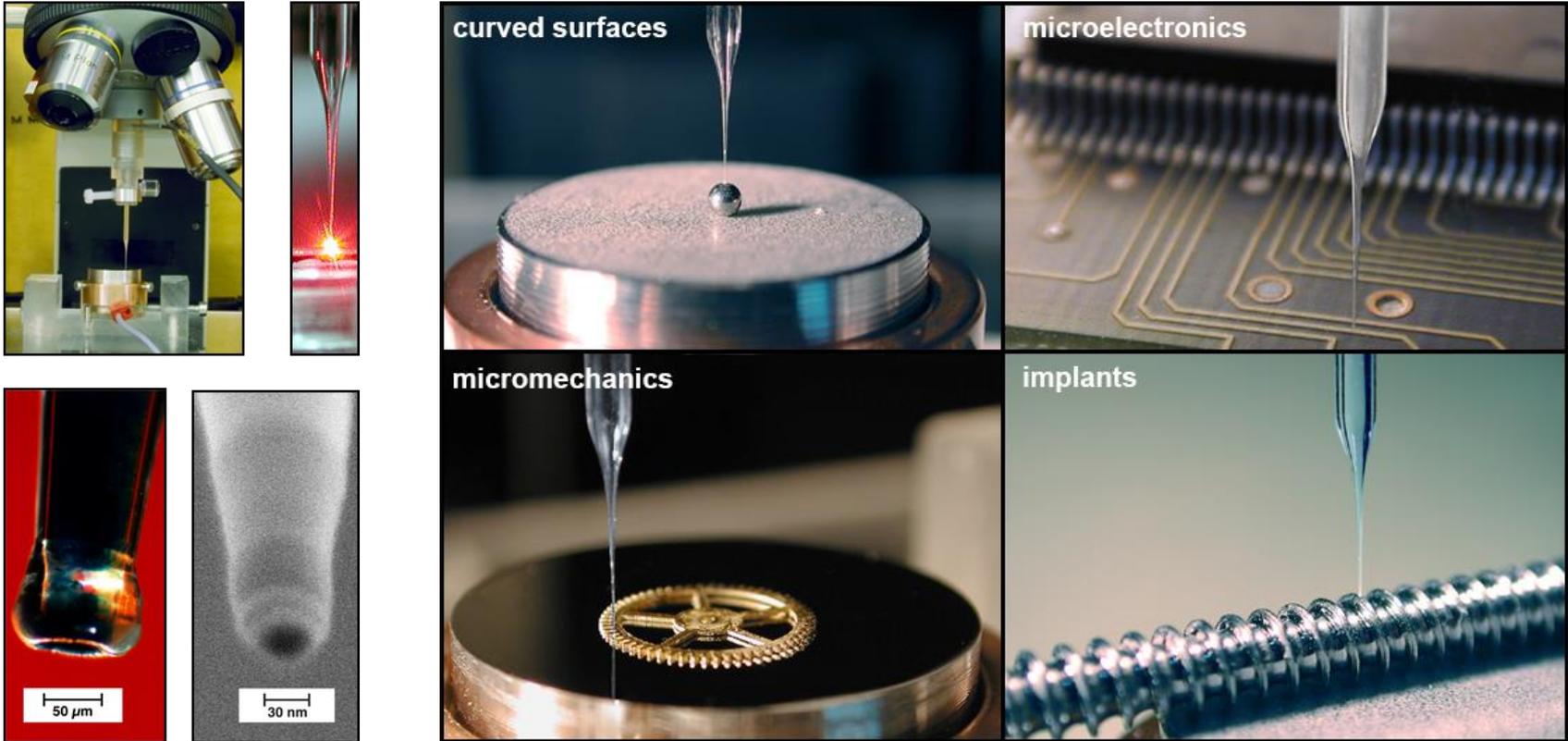
60 microns foil

No heat affect on nano Al base material



250 microns foil

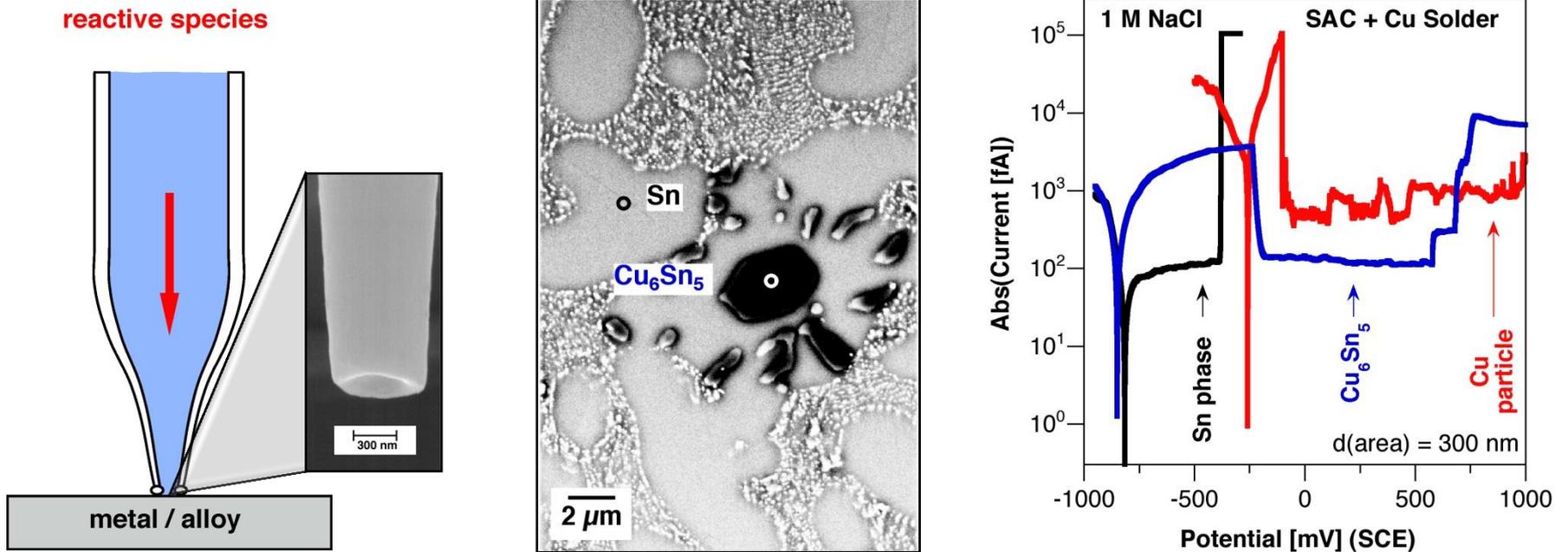
Heat affected zone < 200 μm



In-house developed micro-capillary electrochemical setups can:

- Compare corrosion-susceptibility of different microstructural features in joint zone.
- Determine corrosion rate of the most susceptible microstructural feature in joint zone.
- Identifying the underlying corrosion mechanisms in different harsh environments.

Corrosion resistance of Cu-nanoparticle-reinforced lead-free Sn-Ag-Cu solders



Electrochemical polarization curves, as measured with 300 nm glass-capillary filled with 1 molar NaCl solution on various phases of the Cu-particle-reinforced lead-free Sn-Ag-Cu solder.

- Cu particles are (slightly) active and very noble.
- Sn-phase and Cu_6Sn_5 particles are more passive.

Conclusion: Cu nano-particles can act as local galvanic element, whereas Cu_6Sn_5 particles do not act as local galvanic element. → Cu-nanoparticles should fully react during soldering!

Vielen Dank für Ihre Aufmerksamkeit
Thank you for your attention
Merci pour votre attention

Acknowledgements

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Empa-Colleagues:

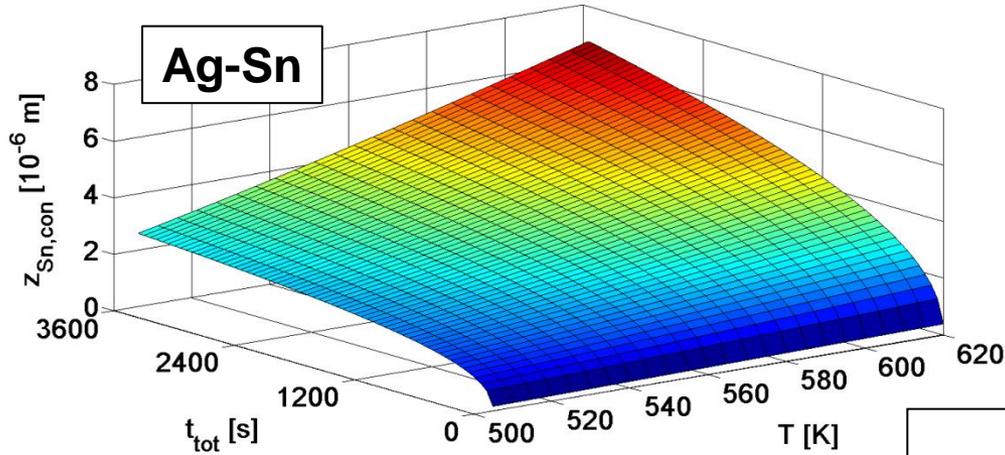
Vincent Bissig, Claudia Cancellieri, Mirco Chiodi, Hans Rudolf Elsener, Roland Hauert, Jacob Kübler, Joanna Lipecka, Adrian Lis, Remi Longtin, Frank Moszner, Jörg Patscheider, Thomas Suter.

Contact details

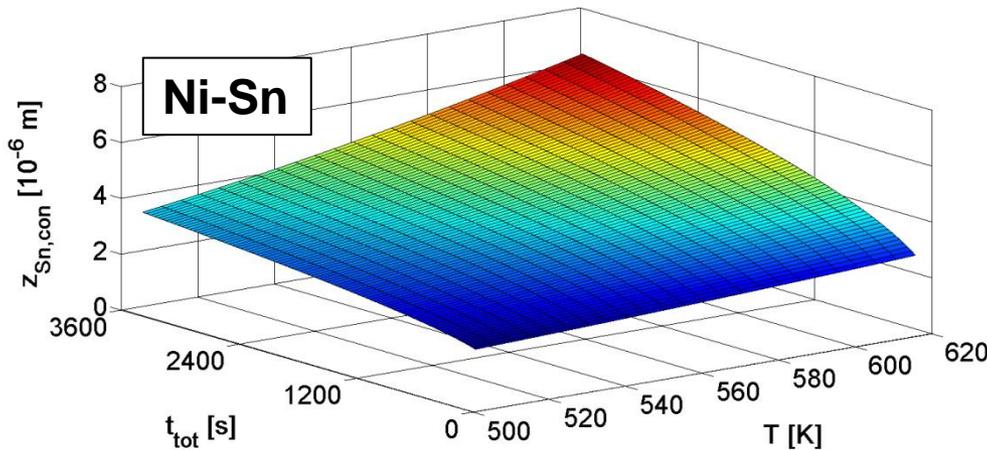
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Homepage: www.empa.ch/Abt202

Constructed Sn-consumption maps



/A. Lis et al., J All Compd 617 (2014) 763/



Example for 7 μ m Sn-foil

Ag_3Sn	235°C	→ 80 min
	300°C	→ 20 min
Ni_3Sn_4	235°C	→ 50 min
	300°C	→ 10 min

$$z_{Sn,con}(T, t) = \left(\frac{\psi}{1 + \psi} \right) \sqrt{k_{0,i} \cdot \exp\left(-\frac{Q_i}{RT}\right) \cdot \sqrt{t}}$$

Sn consumption factor Arrhenius

with $\psi = \frac{(M(Y) \cdot y) / \rho(Y)}{(M(X) \cdot x) / \rho(X)}$

M – molar mass
 ρ – density
 x,y – stoichiometric number

System	Enthalpy of formation (kJ•mol ⁻¹)	Energy Density (kJ•cm ⁻³)	RT ductility	Adiabatic reaction temp.(°C)	Ref.
Pt/Al	-100	1451	-	2800	<i>McAlister 1986</i>
Ni/Zr	-51	1025	-		<i>Nash 1984</i>
Ru/Al	-62	1000	✓		<i>Jung 1992</i>
Ni/Al	-59	861	-	1639	<i>Kleppa 1994</i> <i>Huang 1998</i>
Co/Al	-55	800	-		<i>Kleppa 1994</i>
Ti/Al	-40	788	-	1227	<i>Schuster 2006</i>
Y/Ag	-27	771	✓		<i>Colinet 1995</i>
Ni/Ti	-34	563	✓	1355	
Y/Cu	-19	506	✓		<i>Colinet 1995</i>